NUCOR®

VULCRAFT/VERCO GROUP

Presented By Darrell Marchell, P.E. Business Dev Mgr.

Steel Floor Joist Presentation

Septemeber 28, 2021

Topics:

EOR & Joist Manufacturer's responsibilities

- □Non-composite Joists
- Composite Joists
- □ Joist End Connection Options
- □Software Solutions for Floor Joists



□MEP openings



Specifying Joists:

Building Code:

□ 2018 IBC Section 2207

- References Steel Joist Institute (SJI) Specifications
- SJI Specifications: included in Vulcraft Manual
- IBC Section 2207.4: "Steel joist placement plans do not require the seal and signature of the joist manufacturer's registered design professional."
- Vulcraft & the other manufacturers are SJI members



Specifying Joists:

Engineer's Responsibility:

- Depth of joist and joist girders
- Joist span
- Joist spacing & starting point for layout
- Support / end connection details
- All required loading
 - uniform, concentrated, axial, etc.

- Serviceability constraints
 - Deflection Criteria is most common.
- Any additional geometry considerations
 - Special sprinkler considerations, etc.



Specifying Joists

Vulcraft's Responsibility:

- Furnish Placement plans.
- □ Placement plans serve 2 purposes:
 - Shows all required loading, so Engineer can review & confirm.
 - Shows mark number & location for erection purposes.
- Determine sizes of all joist or joist girder members.
 - Top & Bottom Chord angles, Web sizes, Seat angles, etc.
 - Determine Weld sizes for webs
- Furnish stamped & signed joist calculations.
 - Calculation printed at time of fabrication.
- □ Fabricate the joists.

Floor Joist History:

□ Original use – joists 2' to 4' o.c. with form deck

- Joists initially limited end reactions, 9K and total load, 550 plf
- Topping slab must fit occupancy use especially serviceability
- Still good solution for 125 psf, 250 psf storage applications

□ LH-Series with 1.5B Formlok deck (1970s)

- Joist spacing increased to 6' to 7'-6"
- Common loading 100 psf live load, 75 psf dead load
- Joist girders used in lieu of steel beams as primary members
- Load per foot designation, such as 32LH1050/600

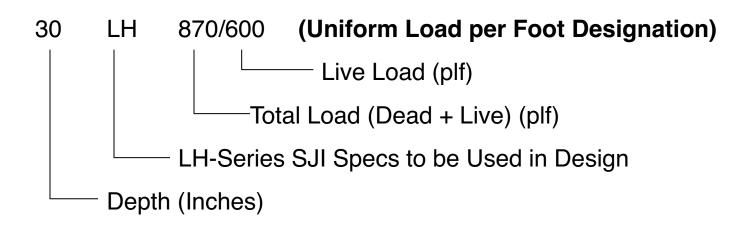
□ LH-Series with W2 or W3 decks (1980s)

- Standard SJI Joist Tables load range not adequate for wider spacings, tables were structured mostly around roof loadings
- Load per foot joists used, TL/LL in plf after Depth
- Bolted flush frames first used on joists

□ LH-Series Joists with Expanded Load Tables (2020)

- Joist spans from 12x depth to 24x depth
- 18 inch joist has total load/ live load in plf listed from 18' to 36'
- Upper limit on loads is generally slightly above 2900 plf
- Joist depths from 18 to 48 inches, spans 18' to 96'

Uniform Load per Foot Designations:



- □ **<u>Best</u>** way to designate joist
- □ LH joists with Uniform Load per foot designation:
 - Available in full inch depths
 - 28LH, 29LH, 30LH,...

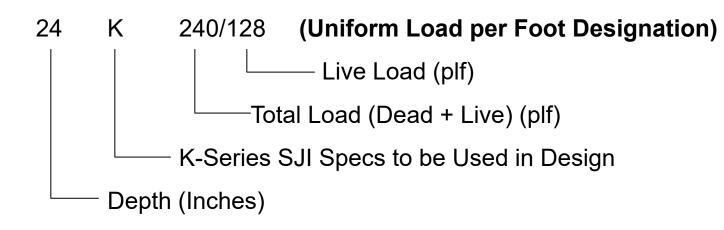
LH Expanded Load Tables:

ASD

STANDARD LOAD TABLE/OPEN WEB STEEL JOISTS, LH-SERIES Based on a 50 ksi Maximum Yield Strength - Loads Shown In Pounds Per Linear Foot (plf)																			
Joist																			
	18LH02	18LH03	18LH04	18LH05	18LH06	18LH07	18LH08	18LH09	18LH10	18LH11	18LH12	18LH13	18LH14	18LH15	18LH16	18LH17	18LH18	18LH19	18LH20
Designation																			
Depth (in.)	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18	18
Approx. Wt.	10	11	12	14	15	17	19	21	23	25	28	33	36	39	44	50	57	62	83
(lbs./ft.)	10		12	17	15		15	- 1	23	25	20	55	50	35		50	51	02	05
Span (ft.)																			
+																			
18	805	896	1039	1175	1438	1529	1728	1989	2231	2489	2751								
	805	896	1039	1175	1438	1529	1728	1889	2231	2489	2751								
19	748	833	966	1093	1329	1414	1598	1831	2054	2291	2533								
20	748 697	833 776	966 899	1093 1018	1329 1231	1414	1500 1480	1601	2054 1895	2291	2533 2337	2805							
20	697 696	774	899	1018	1231	1310 1229	1480	1688 1369	1895	2114 2005	2337	2805							
21	649	723	838	949	1143	1229	1283	1562	1752	1955	2161	2587	2825						
21	600	667	772	870	1008	1059	1105	1180	1565	1728	1918	2220	2413						
22	606	675	783	886	1063	1130	1277	1448	1624	1812	2003	2391	2612	2829					
	520	579	670	755	874	919	959	1024	1358	1500	1664	1926	2094	2276					
23	567	631	732	829	990	1053	1189	1345	1508	1683	1860	2216	2420	2622					
	454	505	585	659	764	803	838	894	1186	1310	1454	1683	1829	1987					
24	531	591	685	776	924	982	1110	1250	1403	1566	1732	2059	2248	2436	2811				
	399	444	514	579	671	705	736	786	1042	1151	1277	1478	1607	1746	1922				
25	497	554	643	728	863	918	1037	1167	1309	1461	1615	1916	2093	2268	2587	2950			
	353	392	454	511	593	623	650	694	920	1016	1128	1306	1419	1542	1697	1929			
26	468	521	604	684	809	840	876	936	1223	1365	1509	1788	1953	2115	2390	2725			
07	313	348 493	403 571	454	526 749	553	577	616	817	902	1001	1159	1260	1369	1506	1712	2016		
27	442 284	493 317	5/1 367	648 414	469	809 513	843 534	901 571	1145 728	1278 804	1413 893	1671 1033	1825 1123	1978 1220	2214 1343	2524 1526	2916 1739		
28	418	467	535	614	696	780	812	868	1074	1198	1325	1565	1710	1852	2057	2345	2709		
20	259	289	329	378	419	476	496	527	652	720	799	925	1006	1093	1203	1367	1557		
29	391	438	500	581	648	726	784	838	1009	1126	1245	1469	1604	1738	1916	2184	2523	2811	
	234	262	296	345	377	428	462	491	586	647	718	832	904	982	1081	1229	1400	1538	
30	367	409	469	543	605	678	758	810	949	1059	1171	1380	1508	1634	1789	2039	2356	2624	
	212	236	266	311	340	386	427	458	529	584	648	750	816	886	975	1108	1263	1387	
31	345	382	440	508	566	635	717	783	894	996	1104	1300	1420	1538	1674	1909	2205	2456	
	193	213	242	282	307	349	387	418	479	529	587	679	738	802	883	1003	1143	1256	
32	324	359	413	476	531	595	680	759	844	934	1042	1226	1336	1451	1570	1790	2068	2303	2862
00	175	194	219	256	280	317	351	380	435	480	533	617	671	729	802	911	1038	1141	1402
33	306	337	388	448	499	559	641	713	798	878	980	1157	1255	1370	1475	1682	1943	2164	2689
34	160 289	177 317	200 365	233 421	254 470	288 526	320 604	346 671	396 754	437 826	485 923	562 1089	611 1182	664 1291	731 1389	830 1584	946 1829	1039 2038	1277 2532
34	289 147	317 161	365 182	421 212	232	526 264	292	316	362	826 399	923 443	1089 513	558	1291 606	1389 667	1584 758	1829 864	2038 949	2532
35	273	299	344	397	443	496	571	633	711	779	870	1027	1114	1217	1310	1494	1725	1922	2388
	135	148	167	195	212	241	267	289	331	366	406	470	511	555	611	695	791	869	1068
36	259	283	325	375	418	469	540	598	672	736	822	970	1053	1150	1237	1411	1630	1816	2256
	124	136	153	179	195	222	246	266	304	336	373	432	469	510	561	638	727	798	981

□ Can be used to help approximate self-weight of joist

Uniform Load per Foot Designations:



□ Limited to 550plf total load

□ K series depths:

• Available in 2" depth increments from 10" to 30"



There are 2 options for composite joists:

□CJ series composite joists:

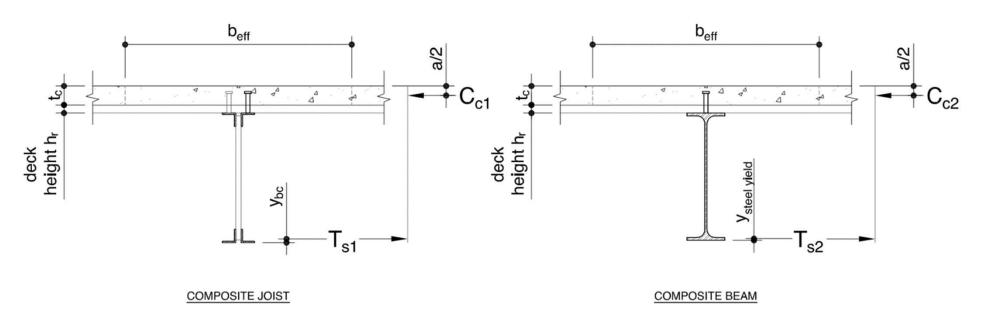
Welded Shear Studs for composite action

□Ecospan E series composite joists:

- Shearflex Screw for composite action
 - Self-drilling/Self-tapping screw
- IAPMO ER 366

□Same design principles as Composite Beam

- Concrete over steel deck used for compression
- Bottom flange/chord steel used for tension
- Nelson[®] studs used for shear transfer CJ Series
- Shearflex screws used for shear transfer Ecospan



□ Composite joists can be shallower than non-composite joists,

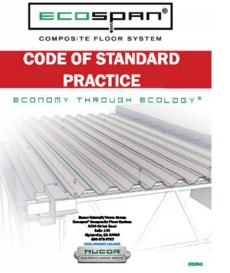
- Composite Joists: span 30x depth
- Non-Composite Joists: span 24x depth
- Lighter than same depth non-composite joist
 - Top chord less area, larger effective depth

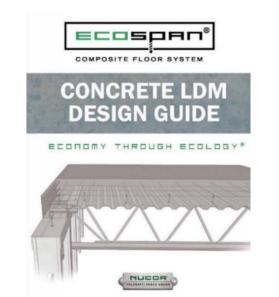
□ Weld Studs or Shearflex screws attached in staggered pattern

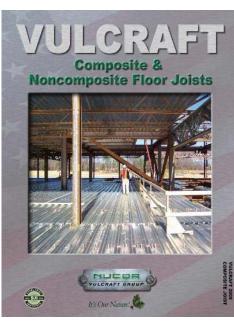
activates both chord angles

- Composite Joist & Ecospan catalogs available online
 - contains load tables, checklist, SJI specification for joists.
 - https://vulcraft.com/Literature







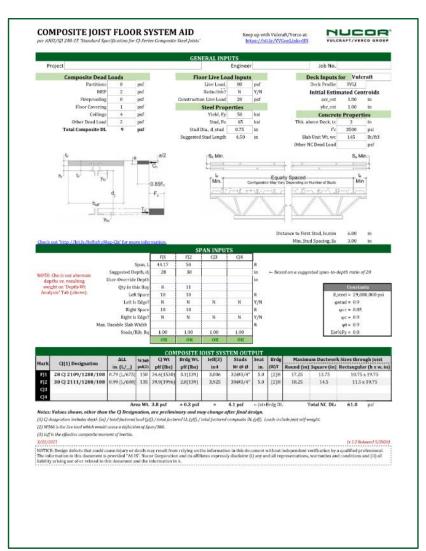


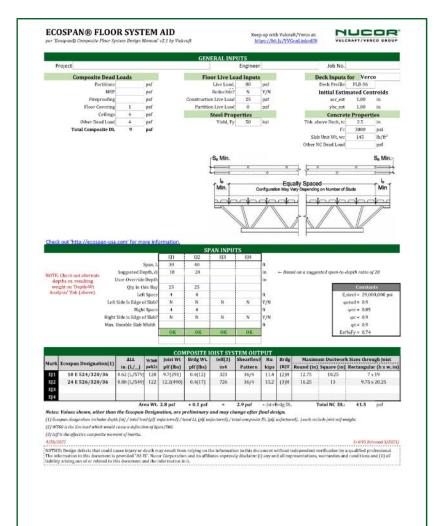


Composite Joist Online Tools:

CJ Series: Composite Joist Floor System Aid

□Ecospan: Ecospan Floor System Estimating Aid





6

C²

U

UL

Additional Info on Plans:

□ Deck spec:

- Ecospan: Verco BFormlok deck
- CJ: Verco B, W2, or W3 deck

□ Concrete spec:

- Slab Thickness above the deck
- Concrete unit weight (pcf)
- Concrete Compressive Strength f'_c
 - 3.0ksi-5ksi typical

Additional Info on Plans:

For both Ecospan & CJ series:

□ Construction Live Load:

- Call out the psf loading.
- 20 psf to 75 psf.
- Live Load depends on how slab finished.
 - Manual Tools vs. Motorized Equipment

Needed for Pre-Composite check

Add'l Info: Deflection Criteria:

Live Load Deflection Criteria Only

□SJI Specifications only require LL deflection

□IBC Table 1604.3:

- Per footnote d & g: D+L check is for creep
- Steel Structural Members, D = 0 for creep
- So only LL deflection needed for steel joists or joist girders

□Specialty cases may have add'l deflection criteria

Camber can be used to offset most/all Dead Load Deflection

VULCRAFT/VERCO GROUP

Composite Joist Camber:

CJ Series Camber:

□ Engineer to specify % of load for camber:

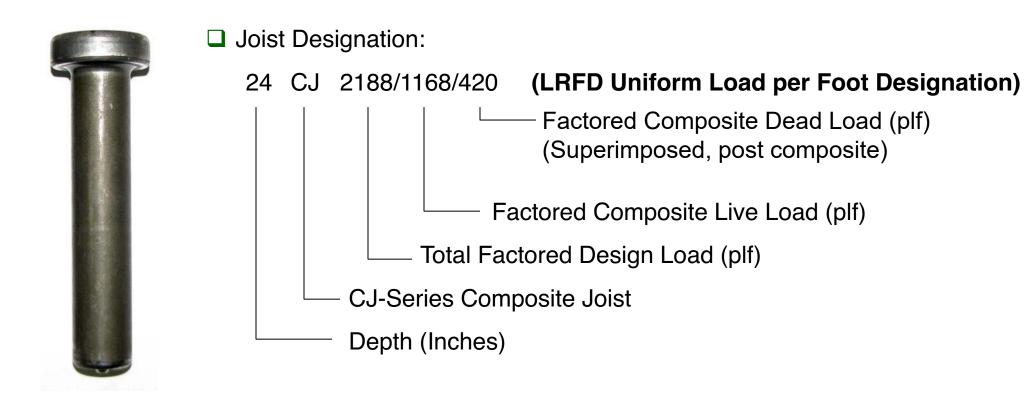
- Non-Composite Dead Load (typically 100%)
- Composite Dead Load (typically 0%-50%)
- Composite Live Load (typically 0%-25%)

Ecospan Camber:

Standard SJI Camber common due to shorter spans



CJ-Series Designations:



CJ joists use factored loads for designationOnline Design tool to help specify

CJ Series: Shear Studs:

TABLE 103.5-1

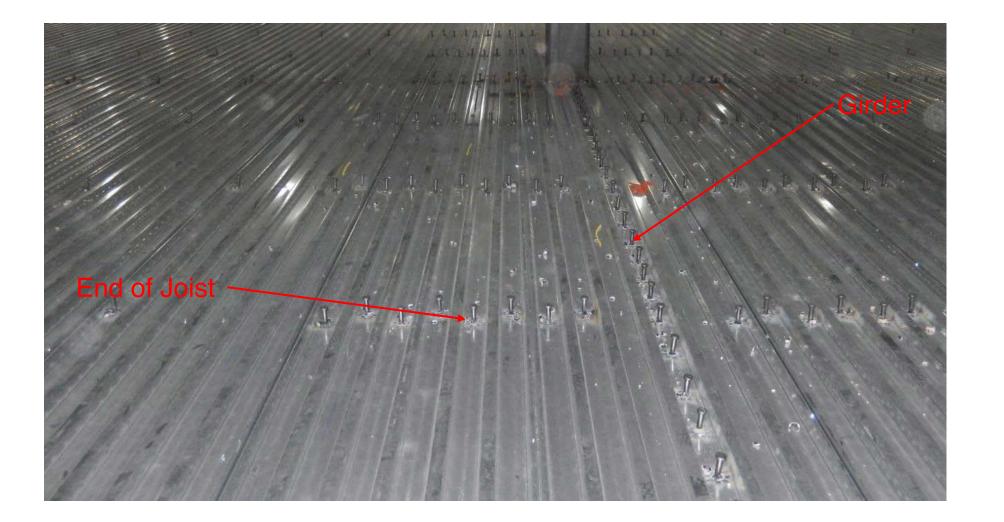
MINIMUM TOP CHORD SIZES FOR INSTALLING WELDED SHEAR STUDS

Shear Stud Diameter in. (mm)	Minimum Horizontal Flat Leg Width in. (mm)	Minimum Leg Thickness in. (mm)
0.375 (10)	1.50 (38)	0.125 (3.2)
0.500 (13)	1.75 (44)	0.167 (4.2)
0.625 (16)	2.00 (51)	0.209 (5.3)
0.750 (19)	2.50 (64)	0.250 (6.3)

□ Top chord angle size & thickness also dependent on stud diameter

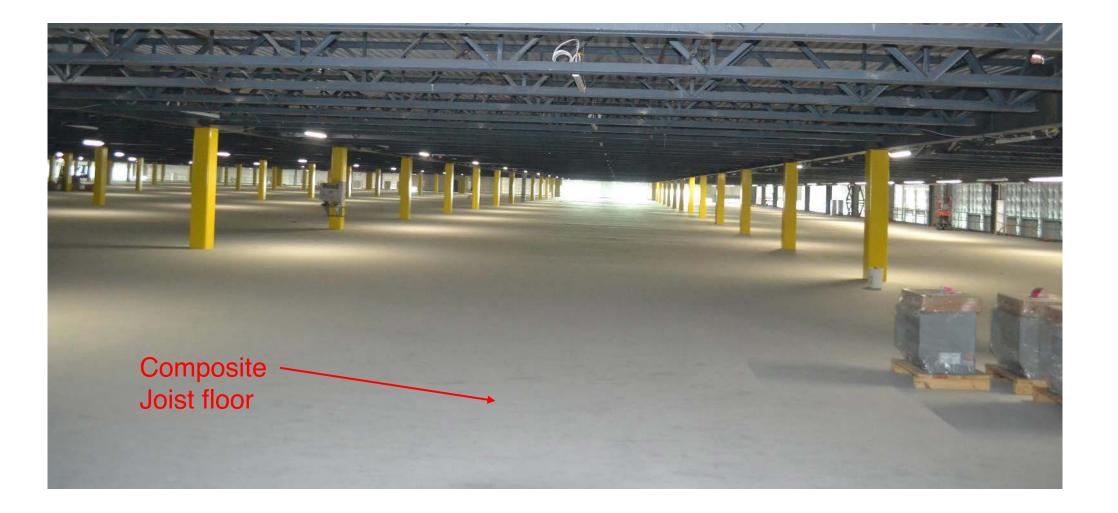
- SJI allows: Stud diameter / 3 for min. thickness
- Less stringent than AISC, SJI controls for joist

CJ Series: Shear Studs



VULCRAFT/VERCO GROUP

CJ Joists:



VULC

Ecospan Composite Joist System:

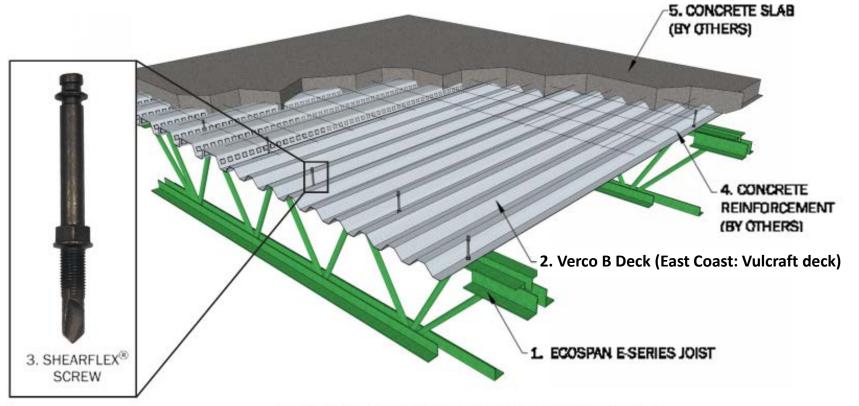


Figure 1-1: The Ecospan® Composite Floor System

V U L

Common Ecospan Projects:

MULTI-STORY RESIDENTIAL

APARTMENTS / CONDOS SENIOR HOUSING HOTELS / RESORTS DORMITORIES / MILITARY HOUSING

OFFICE - COMMERCIAL

OFFICE BUILDINGS SCHOOLS (Private or outside California) MEZZANINES

Ecospan Composite Joists:



L L

□ Joists from Exterior Wall to Corridor Wall

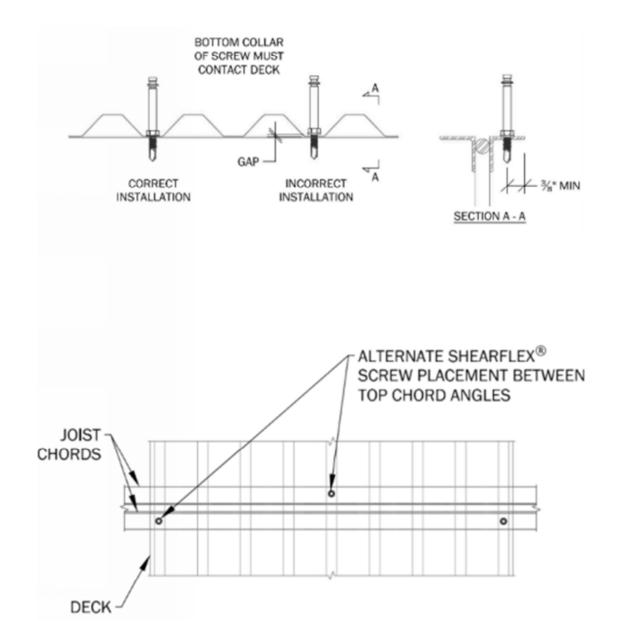
- Partitions are non-bearing
- W deck at corridor

Ecospan Composite Joists:



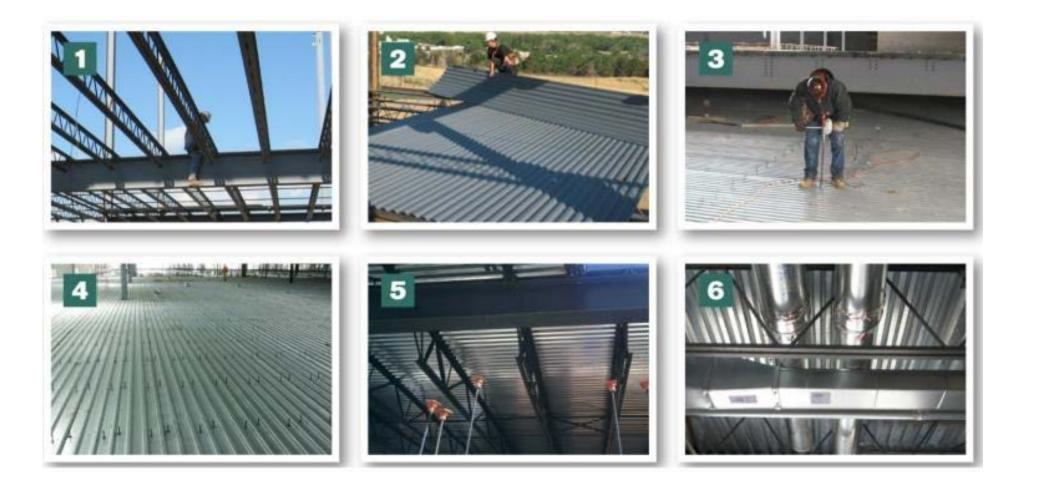
• Corridor with just 'W' deck

Ecospan Composite Joist System:



VULCRAFT/VERCO GROUP

Ecospan Composite Joist System:



Б

E-Series Designations:



24 E	488/220/60 (Uniform Load per Foot Designation, unfactored)							
	Composite Dead Load (plf) (Superimposed, post composite)							
	Composite Live Load (plf)							
	Total Design Load (plf)							
	 Ecospan E-Series Composite Joist 							
	 Depth (Inches) 							

Ecospan E joists use unfactored loads
 Number of Shearflex Screws by Vulcraft
 Online Design Tool to help specify

Ecospan Composite Joists:

	E-Serie	s Joist N	laximun	n Span C	hart (ft)					
Typical Loading	Live Load NC Dead I	= 112 PSF	SF	Commercial Loading Total Load = 158 PSF Live Load = 100 PSF NC Dead Load = 43 PSF						
Depth	On Center Joist Spacing									
(in)	4'-0"	4'-6"	5'-0"	4'-0"	5'-0"	6'-0"				
Typical Loading (plf)	448/220/60	505/248/68	560/275/75	632/400/60	790/500/75	948/600/90				
10E	25'	25'	25'	25'	21'	17'				
12E	30'	30'	30'	30'	25'	21'				
14E	35'	35'	35'	35'	29'	24'				
16E	40'	40'	39'	37'	33'	27'				
18E	45'	44'	42'	39'	35'	31'				
20E	50'	47'	44'	41'	37'	32'				
22E	52'	49'	46'	43'	38'	33'				
24E	54'	51'	48'	45'	40'	36'				
26E	57'	53'	50'	47'	41'	38'				
28E	59'	55'	52'	49'	43'	39'				
30E	60'	57'	54'	50'	45'	41'				

Notes:

1. Assumed 36/4 attachment pattern

2. Assumed 1.0C24 (3.5" total) for Residential

3. Assumed 1.5VL22 (4.0" total) for Commercial

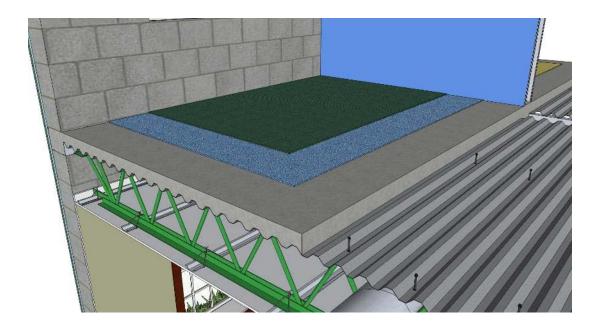
4. Joists ranging from 10"-14" deep are assumed rod web joists, while joists 16"-

30" may be crimped or uncrimped angle web joists

Ecospan Sound Ratings:

Sound Attenuation

- □Sound Transmission Classification (STC)
- □Impact Insulation Classification (IIC)
- □ Meets or Exceed IBC req'ts with common materials



Full Scale Tests							
Flooring Materials/Thickness	IIC	STC					
Bare Concrete	26, 30*	57					
Carpet 1. 6PCF Pad (0.4") 2. 100% Pet Polyester Carpet (0.438")	77	57					
Ceramic Tile 1. Loose-laid Cork (0.235") 2. Thinset Mortar 3. Glazed Ceramic Tile (0.3")	51, 54*	Not Tested					
Wood Laminate 1. Underlayment (0.07") 2. Wood Laminate Floor (0.38")	54	Not Tested					
*Resilient sound isolation clips (RSIC-1) used Table 4-							

*Resilient sound isolation clips (RSIC-1) used in place of wire ties.

Ecospan UL Ratings:

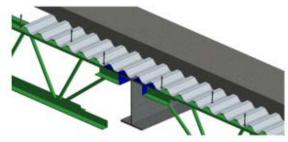
Common UL listings

UL Fire Ratings							
UL Code	Application						
*Design No. G561	Direct Applied and/or Suspended Gypsum Board Ceiling						
Design No. G213	Suspended Acoustical Ceiling						
Design No. G227	Suspended Acoustical Ceiling						
*Design No. G229	Suspended Acoustical Ceiling						
Design No. G236	Suspended Acoustical Ceiling						
Design No. G243	Suspended Acoustical Ceiling						
Design No. G222	Suspended Gypsum Board Ceiling						
Design No. G547	Suspended Gypsum Board Ceiling						
*Design No. G710	Spray-on Fire Proofing						
Design No. N789	Spray-on Fire Proofing						
*Design No. D902	Unprotected Comp. Deck in Corridor Areas						
*Design No. D916	Unprotected Comp. Deck in Corridor Areas						
Design No. D918	Unprotected Comp. Deck in Corridor Areas						
Design No. D919	Unprotected Comp. Deck in Corridor Areas						

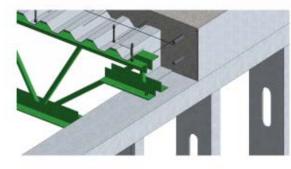
*Most commonly utilized UL Ratings

Table 4-1

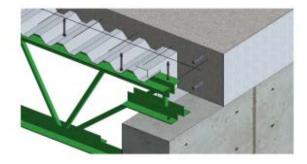
Ecospan Composite Joists:



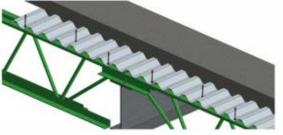
Flush Seat on Steel



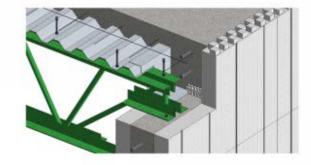
Cold Formed Steel



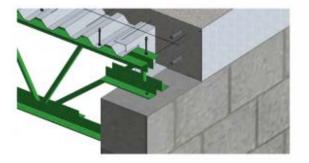
Concrete



Standard Seat on Steel



Insulated Concrete Forms

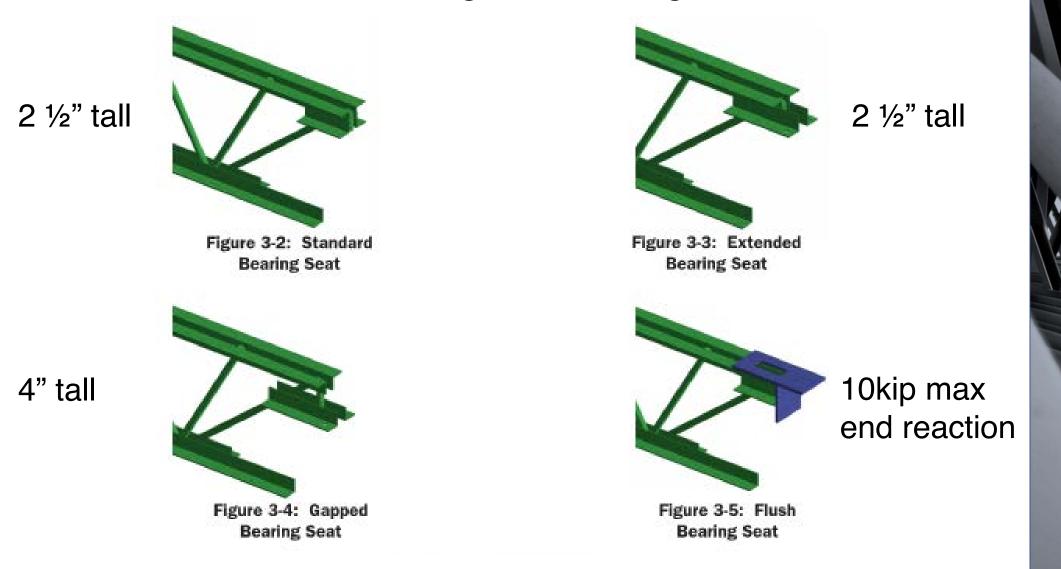


Masonry



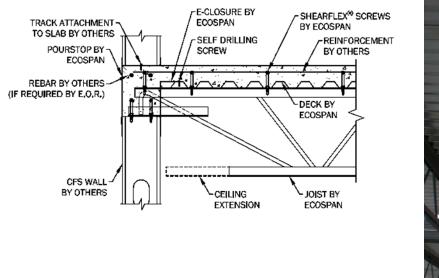
Ecospan Joist Seats:

E-Series Joist Bearing Seat Configurations:



Ecospan Joist Seats:

NOT TO SCALE



DEEP JOIST SEAT ON CFS

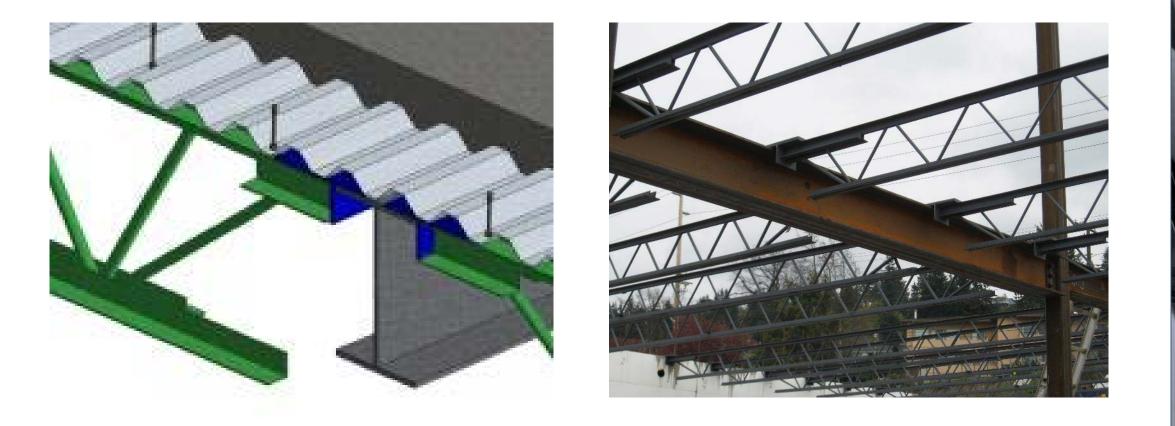
(3.2)



Θ

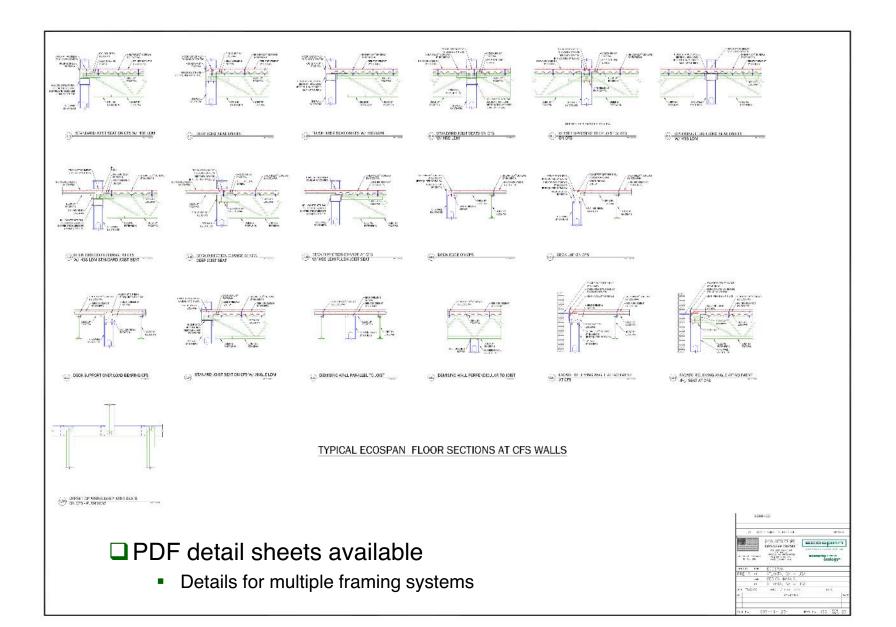
VULCRA

Ecospan Joist Seats:



Ecospan Flush Joist Seat

Ecospan System Details:



0

O GR

22

m

4

œ

U

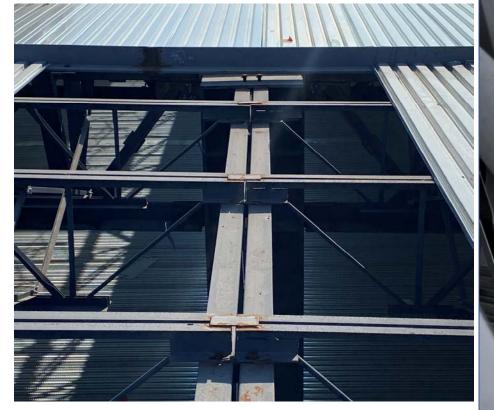
VUL

Joist End Connection:

At Concrete / Masonry wall

- Standard seat probably best
- Can connect to ledger or pocket
- Standard seat can take axial load

□ Standard seat at Joist Girder



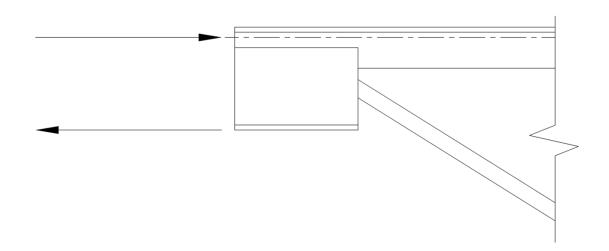
Axial Load Thru Seat:

Joists:

- 2 ½" deep seat: 26
- 5" deep seat:

26k ASD (E = 36.4k)20k ASD (E = 28.0k)

As the joist seat gets deeper, capacity decreases.



VULCRAFT/VERCO GROUP

Axial Loads:

□More common on Non-composite projects

□State axial loads in code terms

- \blacksquare E, E_m, W, 0.7E, 0.7E_m , or 0.6W
- Do not simply say "axial load"
- $\square Specify E_m \& 0.7E_m \text{ loads}$
 - do not specify E or 0.7E load and say to multiply by $\Omega_{\rm o}$

□Max Axial Capacities:

Joist Type		Top Chord Seismic Axial Loads (ASD)*
K	2.5" & 3"	55 kips
LH	3"	100 kips
LH	5"	450 kips **

*Max axial capacity will vary slightly depending on the vertical loads on the joist

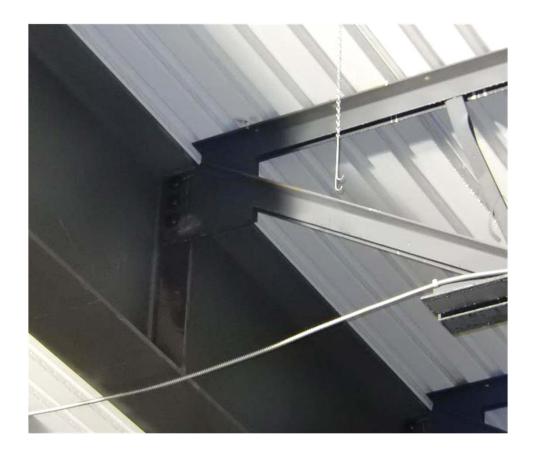
**The connection between the joists may control when there are large axial loads.

Joist End Connection:

Wide Flange Girders: LH & CJ Series

Bolted Flushed Framed End connection is great option





Bolted Flushed Framed End Connection:

□ Benefits:

- Deeper Girder
- Composite Girders
- Installation similar to Steel Beams
- Blocking not required between joists
- Significant improvement in Vibrational performance

Draw Back:

- No axial load thru bolted plate
- Not enough weld from plate to top chord for eccentricity



Bolted Flushed Framed End Connection:

□ Bolts:

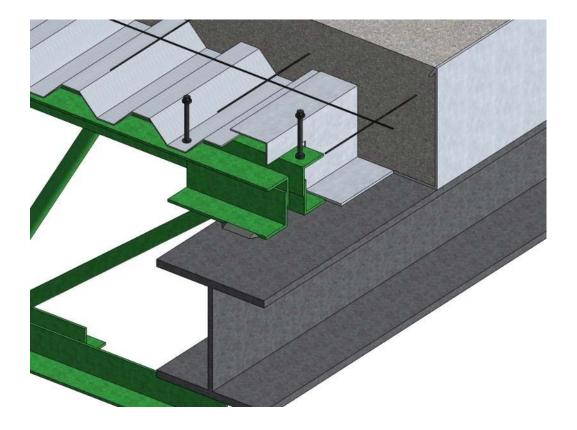
- High Strength Bolts (A325 or A490)
- 1" Diameter min recommended
- Fully Tensioned Bearing Connection
- Spacing & Edge distances by project Engineer

□ Slip Critical Bolts issues:

- Add'l cost for req'd surface prep of plate
- Add'l cost to protect plate when priming joist

Joist End Connection

- □ Wide Flange Girders: Ecospan
 - Standard Joist Seat with E-Closure
 - Flushed Joist Seat





Software Solutions

□Vulcraft Design Tools

- CJ Series: Composite Joist Floor System Aid
- Ecospan: Ecospan Floor System Estimating Aid

RAM Steel

- Expanded Non-composite joist tables
- Includes camber in deflection calculations
- Currently does not have composite joists

- Composite joists in program
- Expanded load tables & deflection with camber in upcoming version 16 release

Software Solutions

Vibration:

- Neither RAM or RISA have Bolted Flush Framed Connections in their Vibration analysis
 - Standard joists seat will yield higher accelerations than Bolted Flushed Frame End Connections.
 - The difference between Standard seat & Bolted Flush Framed End Connection can be the difference of the floor satisfying the criteria or not.
- □ Vulcraft Vibration Analysis Walking
 - Includes Bolted Flushed Frame End Connections.
 - Includes Ecospan Flush Joist Seat.
 - Free Online Design tool

				V	IBRATIO
ation Walking	Calculation & Output	Design Aid Info	Design Aid Diagrams	Technical Revisio	on
	Keep up with V	'ulcraft by following us at	https://www.linkedin.com	n/company/vulcraft	-division-of-nucor-steel/
	n Analysis Tool - Wal 1 Digest 5: Vibration of Steel Jo		ors 2015	0	
AISC Steel D	esign Guide 11: Vibrations of	Steel-Framed Structura	al Systems Dues to Human	Activity 2nd Edition	n 2016
-	Girders are both treated as simple a more complex floor system, l			lyze a floor for vibrati	on from something other th
2) If you have it is recomm 3) Prompts fo The latest op	-	ike continuous joists or g nalysis. <u>https:/</u> are dynamic and will cha wn when it is selected. It	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo	made. Some of the drop of the latest options to	op down menus are dynami appear.
 If you have it is recommendation Prompts for The latest op 	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h	ike continuous joists or g nalysis. <u>https:/</u> are dynamic and will cha wn when it is selected. It	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo	made. Some of the drop of the latest options to	op down menus are dynamic appear.
 2) If you have it is recommondary 3) Prompts for The latest op 4) Pop-up Composition Project Information 	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h rmation:	ike continuous joists or g nalysis. <u>https:/</u> are dynamic and will cha wn when it is selected. It	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo	made. Some of the drop of the latest options to	op down menus are dynamic appear.
 2) If you have it is recommu- 3) Prompts for The latest op 4) Pop-up Cor <u>Project Infor</u> <i>Project</i> 	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dow mments have been provided to h rmation:	ike continuous joists or g nalysis. <u>https:/</u> are dynamic and will cha wn when it is selected. It	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo	made. Some of the drop of the latest options to	op down menus are dynamio appear. 'alues.
 2) If you have it is recommendation 3) Prompts for The latest ope 4) Pop-up Commendation 4) Project Information Project Engineer 	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h rmation:	ike continuous joists or g nalysis. <u>https:/</u> are dynamic and will cha wn when it is selected. It	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo	made. Some of the drop of the latest options to	op down menus are dynamio appear. 'alues.
2) If you have it is recomm 3) Prompts for The latest op 4) Pop-up Cor <u>Project Infor</u> <i>Project</i> Engineer Floor Inform	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h rmation: Vibration Analysis hation: Bay Info: Line Occupancy: Office - Electronic	ike continuous joists or g nalysis. <u>https:/</u> are dynamic and will cha wn when it is selected. It	irders, or if you need to ana //www.floorvibe.com/wp/ inge based on the selections may take a second or two fo information needs to be pro-	made. Some of the drop of the latest options to	op down menus are dynami appear. ralues. Job No. 20-
2) If you have it is recomm 3) Prompts for The latest op 4) Pop-up Cor <u>Project Infor</u> <i>Project</i> Engineer Floor Inform	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h rmation: Vibration Analysis ration: Bay Info: Line Occupancy: Office - Electronic <u>Modal Damping Work-up Aid</u>	ike continuous joists or g nalysis. <u>https://</u> are dynamic and will cha wn when it is selected. It nelp aid the user on what i	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo information needs to be pro-	made. Some of the dro r the latest options to vided or appropriate v	op down menus are dynamic appear. ralues. Job No. 20- a_0 /g = 0.50% to 0.55
2) If you have it is recommo 3) Prompts for The latest op 4) Pop-up Con <u>Project Infor</u> Project Engineer Floor Inform	e a more complex floor system, 1 ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h rmation: Vibration Analysis ration: Bay Info: Line Occupancy: Office - Electronic <u>Modal Damping Work-up Aid</u>	ike continuous joists or g nalysis. <u>https://</u> are dynamic and will cha wn when it is selected. It nelp aid the user on what i elp aid the user on what i Damping Ratio is the sum	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two fo information needs to be pro- formation needs to be pro- not be pro- not be pro- Tolerance .	made. Some of the dro r the latest options to vided or appropriate v	op down menus are dynamic appear. ralues. Job No. 20- $a_0 /g = 0.50\%$ to 0.55 Modal Damping F
2) If you have it is recommo 3) Prompts for The latest op 4) Pop-up Con <u>Project Infor</u> Project Engineer Floor Inform	e a more complex floor system, I ended to use Floorvibe for the ar or input information in this Tool tions will appear in the drop dov mments have been provided to h rmation: Vibration Analysis nation: Bay Info: Line Occupancy: Office - Electronic <u>Modal Damping Work-up Aid</u> The Final Modal I	ike continuous joists or g nalysis. <u>https://</u> are dynamic and will cha wn when it is selected. It nelp aid the user on what i	irders, or if you need to ana //www.floorvibe.com/wp/ unge based on the selections may take a second or two for information needs to be pro- Tolerance . of the Damping from Comp 0.010 0.005	made. Some of the dro r the latest options to vided or appropriate v	op down menus are dynamic appear. ralues.

https://vulcraft.com/DesignTools

Bay Info: Line					
Vibration Occupancy: Office - Electronic 🔹	Tolerance Acceleration Limit:	$a_0 / g = 0.50\%$ to 0.55	5%		
Modal Damping Work-up Aid					
The Final Modal Damping Ratio is the su	am of the Damping from Components	Modal Damping	Ratio Design Note:		
Structural Sys	stem β ₁ = 0.010 🕕	1) Damping Ratio	β has a major impact	on the Fi	nal Bay
Ceiling & Duct Work:	Yes 🔹 🕕		all changes to the Dan		
Ce	eiling $\beta_2 = 0.005$		ct to final acceleration		
	Duct $\beta_3 = 0.005$	the members.	ibers or changing the	moments	of inertia o
	t-Out β + = 0.005		Info tab for addition:	alreferen	ce
Full Height Drywall Partitions in Bay:		information for Da			
i an neight bi y nan a dhono in buy (0				
	0				
Additional Dam	pping $\beta_7 = 0.000$	Constant For	orce P, = 65 lb		
Additional Dam	iping p 7 = 0.000	Constant Por	1001 0 10		
Work-up Total Modal Damping Ratio	$\beta = \Sigma \beta_i = 0.025$				
		Bay Dime	ensions: 🕕		0
USE: Modal Damping	g Ratio β = 0.025 🛛 🕔	Floor V	Width = 150.00	ft	0
		Floor Le	ength = 105.00	ft	0
uperimposed Loading for Vibration Analysis: 🕕 🕕	Deck & Concrete:		·		
	Total Slab Depth				
Dead Load = 4.0 psf 🕕		in Conc. Streng	gth f'c = 3.00 ksi		
Live Load = 8.0 psf 🕕	Deck Height = 1.50	in Conc. Unit W	Veight = 145 pcf		
			A CONTRACTOR OF A CONTRACTOR O		

VULCKAFI

						VIBRATION AN
ation Walking	Calculation Output	Design Aid Info	Design Aid Diagrams Techn	ical Revision		
ration Analys	is Tool - Walking	I	VULCRAFT G	ROUP		
	A CAR IN COMPANY AND A CAR AND A CAR AND A	the user in order to ai	d in the design process:	11100		erance Acceleration
Recommended	Live Loads & Toler ting Vibration Anal	ance Acceleration	Office Fit-Outs & Recom	mended Da		its Table
Table 2 (from SJI T	D5 Table 1.2 & 3.1 - for	walking)	Recommendations from:			
Vibration Occupancy	Recommended Live Load for Vibration Analysis	Tolerance Acceleration Limit ao/g x 100%			opher M. Hewitt and Thomas M. onstruction	
Office - Paper Office - Electronic	11.0 psf 6.0 psf to 8 psf	0.5 to 0.55 0.5 to 0.55	https://www.floorvibe.com Table 3.1	97		
Assembly Area	0.0 psf	0.5 to 0.55	Traditional Office. Full-Height I			
School Church	0.0 psf 0.0 psf	0.5 to 0.55 0.5 to 0.55	WITH suspended ceiling and ductwork attached below the	slab:	mated Damping Ratio β = 0.050	
Shopping Mall	0.0 psf	1.5	Estimated Dead Load:	4 psf	p = 0.000	
Residence	6.0 psf	0.5 to 0.55	Estimated Live Load:	11 psf		
		110-00-00 mo	Estimated partition Load:	4 psf		
	- F2		WITHOUT suspended ceiling		mated Damping Ratio	
			ductwork attached below the	and a second second	β = 0.050	
Freeman F Canie	es Joist Maximum		Estimated Dead Load: Estimated Live Load:	4 psf 11 psf		
Moment of Iner			Estimated partition Load:	4 psf		
Table 4			Table 3.2	4 9 3 1		
Joist Depth (in)	Max Ichards (in4)		Electronic Office, Nearly no par	erwork, Limite	d number of file cabinets. No full	
10	55		height partitions			
12	85		WITH suspended ceiling and	Esti	mated Damping Ratio	
14	115		ductwork attached below the	slab:	$\beta = 0.020$ to 0.025	
16	260		Estimated Dead Load:	4 psf		
18	335		Estimated Live Load:	8 psf		4
20 22	575		WITHOUT suspended ceiling ductwork attached below the		mated Damping Ratio B = 0.020	
24	835		Estimated Dead Load:	1-2 psf	p=0.020	
26	985		Estimated Live Load:	8 psf		-
28	1145		Table 3.3			
30	1320	2	Open Office. Cubicles and no fu	ll height partiti	ons,	
the Shearflex screws	tion considerations for s, which are part of the ospan E series joists	-	WITH suspended ceiling and ductwork attached below the Estimated Dead Load		mated Damping Ratio β = 0.025 to 0.030	
have a maximum top	o chord angle thickness		Estimated Live Load:	8 psf		
of 5/16*. The above inertia for E-series j limitation.	maximum moments of pists reflect this		WITHOUT suspended ceiling ductwork attached below the Estimated Dead Load:		mated Damping Ratio β = 0.020 to 0.025	
			Estimated Live Load:	8 psf		
	osite Joist Moment		Table 3.4	-		
of Inertia:			Office Library, Full-height book			
CI-series joists use h	eaded weld studs for		WITH suspended ceiling and	Esti	mated Damping Ratio	

Floor Information:						
Bay Info: Line						
Vibration Occupancy: Office - Electronic 🔹	Tolerance Acceleration Lin	nit: $a_0/g = 0$.50% to 0.55%			
Modal Damping Work-up Aid						
The Final Modal Damping Ratio is the su	m of the Damping from Components	Mo	dal Damping Ratio De	sign Note:		
Structural Syst	em β ₁ = 0.010	1) [Damping Ratio β has a m	najor impact	on the Fir	nalBay
Ceiling & Duct Work:			eleration. Small change			
	$ling \beta_2 = 0.005$		ch larger impact to final			
	$Duct \beta_3 = 0.005$		ds on the members or cl members.	nanging the	moments	ofinertia of
	$Out \beta_4 = 0.005$	1.000	See Design Aid Info tab	for addition	alreferend	re .
Full Height Drywall Partitions in Bay:			ormation for Damping R			
	Bay $\beta_5 = 0.020$					
Tartitions in	Day p 5 - 0.020					
Additional Dam			Constant Force P. = 6	5 115		
Additional Damp	5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		constant force 1 0 = 0	0 10		
Work-up Total Modal Damping Ratio	$\beta = \Sigma \beta_{i} = 0.045$ (1)					
			Bay Dimensions:	0		0
USE: Modal Damping	Ratio β = 0.045 🛛 🕕		Floor Width =	150.00	ft	0
2			Floor Length =	105.00	ft	0
Superimposed Loading for Vibration Analysis:	Deck & Concrete:					
	Total Slab Depth		_			
Dead Load = 4.0 psf 🕕	(including deck) d = 5.0	00 in	Conc. Strength f 'c =	3.00 ksi		
Live Load = 8.0 psf 🕕	Deck Height = 1.5	50 in	Conc. Unit Weight =	145 pcf		
Collateral Load = 4.0 psf	Deck Self-weight = 2.	3 psf	Conc. Slab Weight =	48.7 psf	0	

□Actual loads on floor (daily basis):

Not code level loads

Bay Dimensions:

Generation Floor Width:

- Distance Perpendicular to Joist span
- Framing is identical or nearly identical
- Size, spacing, length, etc

Given Strength:

- Distance Perpendicular to Girder span
- Framing is identical or nearly identical
- Size, spacing, length, etc

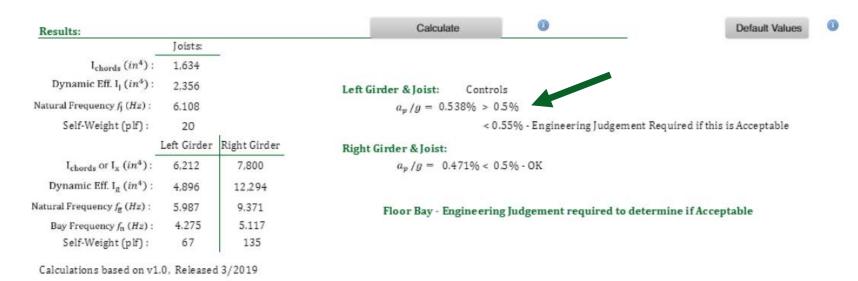
Joist Girde		'Depth' G '#Spaces' N example: 48G 7N 10.7	TotalLoad'/ 'Live Load' (load /4.8 K	s in kips, unfactored)	
Left Girder :			<u>Right Girder :</u>		Input Note:
Girder Type :	Joist Girder	•	Girder Type : Joist Gi	irder 🔻	Due to the number of options that are selection dependent,
Edge Girder :	No	•	Edge Girder : No	•	may take a second or two for the tool to update the display
		0		0	
Designation :		38.4 / 24.0 K			24.0 K
) Span =			Designation : 44 G Span = 30.0 For Girder Tributary V	0 ft	24.0 K
D Span = D J <u>oist Girder D</u> e	30.00 ft		Span = 30.0	0 ft Width:	24.0 K
D Span = D <u>Joist Girder De</u> D Total	30.00 ft		Span = 30.0 For Girder Tributary V	0 ft Width: Girder: Span = 40	
D Span = D J <u>oist Girder De</u> D Total Live	30.00 ft eflection Criteria (for bo Load < L/240	oth girders)	Span = <u>30.0</u> For Girder Tributary V Joist to Left of Left Joist to Right of Right	0 ft Width: Girder: Span = 40).00 ft
D Span = D J <u>oist Girder De</u> D Total Live	30.00 ft eflection Criteria (for bo Load < L/240 Load < L/360	oth girders)	Span = <u>30.0</u> For Girder Tributary V Joist to Left of Left Joist to Right of Right Use Larger Mon	0 ft <u>Width:</u> Girder: Span = 40 Girder: Span = 40 nent of Inertia : Yes).00 ft

Left & Right Girders can be different

<u>Center Joist (joist between girders)</u>	Joist Load/Load De		
Joist Type : LH Series 🔹		actored loads, loads in plf)	
Designation Type : Load/Load 🔻		TotalLoad' / 'Live Load'	
	ex: 24 K 540/400		
Designation: 40 LH 960 / 60	0 CL (CLuse factored	l loads, loads in plf)	
Span = 40.00 ft			Load'/'Factored Composite Dead Load'
Spacing = 6.00 ft on center	ex: 34CJ 1980/1440		
		use unfactored loads, loads	
		d' / ' Live Load' / 'Composit	te Dead Load'
Joist Web Type : Angle	ex: 14E 632/400/6	0	
Joist Deflection Criteria:	Seat Depth 🛛 🕕	Table 1: Seat Depth	Special End Connections: 🕕
oist Deflection Criteria: Total Load < L/240		Tunical Seat	Special End Connections: 0 If LH, CJ, or deep E joist has a
Total Load < L/240	Left End : 5.00 in	· · · ·	t stranger and stranger
		Joiet Type Typical Seat	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0".
Total Load < L/240 Live Load < L/360	Left End : 5.00 in	Joist Type Typical Seat Depth (in)	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0". If E joist has Flush Joist Seat
Total Load < L/240 Live Load < L/360	Left End : 5.00 in Right End : 5.00 in At Left Girder:	Joist Type Typical Seat Depth (in) K Series 2.5 LH Series 5	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0".
Total Load < L/240 Live Load < L/360 Use Larger Moment of Inertia : No	Left End : 5.00 in Right End : 5.00 in At Left Girder: Cont. Blocking between No V	Joist Type Typical Seat Depth (in) K Series 2.5 LH Series 5 DLH Series 5	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0". If E joist has Flush Joist Seat
Total Load < L/240 Live Load < L/360 Use Larger Moment of Inertia : No ▼	Left End : 5.00 in Right End : 5.00 in At Left Girder:	Joist Type Typical Seat Depth (in) K Series 2.5 LH Series 5	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0". If E joist has Flush Joist Seat
Total Load < L/240 Live Load < L/360 Use Larger Moment of Inertia : No	Left End : 5.00 in Right End : 5.00 in At Left Girder: Cont. Blocking between No V	Joist Type Typical Seat Depth (in) K Series 2.5 LH Series 5 DLH Series 5	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0". If E joist has Flush Joist Seat
Total Load < L/240 Live Load < L/360 Use Larger Moment of Inertia : No ▼	Left End : 5.00 in Right End : 5.00 in At Left Girder: Cont. Blocking between No V () At Right Girder:	Joist Type Typical Seat Depth (in) K Series 2.5 LH Series 5 DLH Series 5 CJ Series 5	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0". If E joist has Flush Joist Seat
Total Load < L/240 Live Load < L/360 Use Larger Moment of Inertia : No ▼	Left End : 5.00 in Right End : 5.00 in At Left Girder: Cont. Blocking between No V () At Right Girder:	Joist Type Typical Seat Depth (in) K Series 2.5 LH Series 5 DLH Series 5 CJ Series 5	If LH, CJ, or deep E joist has a bolted flushed framed end connection, use a Seat Depth = 0". If E joist has Flush Joist Seat

□Handles Special End Connections:

- Bolted Flushed Framed End connection
- Ecospan Flush Seat connection



Acceleration Tolerance Limits:

- AISC DG 11 has lower limit
- SJI TD5 has slightly higher limit for floor with Joist
- Engineer to decide if acceptable when between 2 limits

Recommendations:

Vibration Analysis is an Iterative process. It may take a few revisions to an initial design to find a floor system that meets the acceleration tolerance criteria. This is typical for all floor systems.

The following are recommendations for modifications that can be made to an initial design when the analysis comes back with the acceleration being higher than the Acceleration Tolerance Limit. See "Design Aid Info" tab and "Design Aid Diagrams" tab for additional information and discussions into the items below.

1) Increase the Damping Ratio, if appropriate. Small changes to the Damping Ratio have a major impact on lowering acceleration.

2) Hotels, Multi-family, Dorms, Assisted Living, & Similar, if there are partitions in the bay, including partition in Damping Ratio can have a major impact.

3) Increase the Concrete Strength. This will increase the composite moment of inertia, increase the natural frequency and lower the acceleration.

4) Increase Dead Load, Live Load, or Collateral Load to be used for vibration analysis, if appropriate. Increases resisting weight & lowers acceleration.

5) Use Bolted Flushed Framed End Connection on LH, DLH, CJ, & deep E series joists. Set seat depth to 0". Increases WF or Joist Girder eff. moment of inertia.

6) Use Ecospan Flush Joist Seat on E Series joist, if end reaction is less than 10kips. Increases Girder effective moment of inertia.

7) For standard joist seats, consider providing Continuous Blocking between joists. Increases Girder effective moment of inertia.

8) For Ecospan E joist with seat, consider using Cont. Blocking or E-Closures between joists. Increases Girder effective moment of inertia.

□Order of Recommendations is intentional:

- Earlier recommendations will have biggest impact for least cost
- Listed in descending order of bang for the buck

□ More detailed description on Design Aid Info tab

Engineer :	JIW	Analysis • Off	100 110				Job No. <u>19-0125</u> Page:	
							NUCC	
		sis Tool ·		0			VULCRAFT GE	
					te Slab Floors 2015 & AISC St Juman Activity 2nd Edition 20		VOLCKAFT	COOP
Joists and Gire	ders are bo	th treated as s	imple s	pan (not continuou:	s) in this tool.			
Floor Inform								
		Line B to C fro		2 to 9				
Vibration O	ccupancy:	Office - Electr	onic	-				
Superimpose	d Loading f	or Vibration			Deck & Concrete:			
		2007-00-00	0.07	002	Total Slab Depth	227925	Course Presents 11	
		Dead Load = Live Load =	4.0	psf	(including deck) d = 5. Deck Height = 1.	00 in 50 in	Conc. Strength f'e = 3 Conc. Unit Weight =	
	Coll	ateral Load =	0.0	psf	Deck Self-weight = 2.		Conc. Slab Weight =	
122				1000				and but
M		ing Ratio β = int Force P, =			Floor Width = Floor Length =	150.00 ft 105.00 ft		
		incrorce P _e =	05 10		Pioor Length =	105.00 ft		
Girder Inform							<u></u>	
	44G5N38	4/24K			Right Girder : W36X135			
Edge Girder :	No				Edge Girder: No			
Span =	30.00	ft			Span = 30.00	ft		
Joist Girder D	eflection C	riteria			For Girder Tributary Width	1:		
	Load < L/				Joist to Left of Left Gird		40.00 ft	
	Load < L/				Joist to Right of Right Gird		40.00 ft	
Joist Informat Center Joist (i		en pirders)	401.119	507600	Seat Depth		loist Deflection Criteria	2
Joist Informat Center Joist (j		en girders) Span =	40LH9 40.0	50/600 0 ft	Seat Depth Left End : 5.00	ín	Joist Deflection Criteria Total Load < L/2	
				0 ft				40
		Span =	40.0	0 ft	Left End : 5.00		Total Load < L/ 2	40
		Span =	40.0	0 ft) ft on center	Left End : 5.00 Right End : 5.00	in	Total Load < L/2 Live Load < L/3	:40 :60
		Span =	40.0	0 ft) ft on center Joist tl	Left End : 5.00 Right End : 5.00		Total Load < L/ 2	:40 :60
Center Joist (j Results:	ioist betwee	Span = Spacing =	40.0 6.0	0 ft 0 ft on center Joist tl edge	Left End : 5.00 Right End : 5.00 his bay parallel to free , opening, or exterior : No	in C _j = 2	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results:	ioist betwee	Span = Spacing = I _{cheede} of all	40.0 6.0	0 ft 0 ft on center Joist tl edge	Left End : 5.00 Right End : 5.00 his bay parallel to free , opening, or exterior : No specified as the Minimum requ	in $C_j = 2$ wired on the pl	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results: It is recommo	oist betwee	Span = Spacing = I _{cheede} of all Joists:	40.0 6.0	0 ft) ft on center Joist ti edge and Joist Girders be s	Left End : 5.00 Right End : 5.00 his bay parallel to free , opening, or exterior : No specified as the Minimum req Left Girder	in $C_j = 2$ uired on the pl Right Girder	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results: It is recommo	ended that rds (in ⁴) :	Span = Spacing = I _{cheede} of all Joists: 1,634	40.0 6.0	0 ft 1 ft on center Joist tl edge nd Joist Girders be s	Left End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum requ tes or I _n (in ⁴) : 6,212	in $C_j = 2$ wired on the pl Right Girder 7,800	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j <u>Results:</u> It is recomm I _{cbo} Dynamic Ef	ended that rds (in ⁴) : £ I ₁ (in ⁴) :	Span = Spacing = I _{cheede} of all Joists: 1,634 2,356	40.0 6.0	0 ft) ft on center Joist ti edge nd Joist Girders be s I _{chor} Dynamic	Left End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum requ Left Girder Left Girder is or I_n (n^4) : 6,212 : Eff. I_g (n^4) : 4,896	in <i>C_j</i> = 2 wired on the pl Right Girder 7,800 12,294	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results: It is recomm I _{che} Dynamic Ef	ended that $rds(in^4):$ $f_{1}(in^4):$ $cy f_1(Hz):$	Span = Spacing = I _{chards} of all Joists: 1,634 2,356 6,108	40.0 6.0	0 ft 1 ft on center Joist tl edge and Joist Girders be s Ichor Dynamic Natural Freq	Left End : 5.00 Right End : 5.00 his bay parallel to free , opening, or exterior : No specified as the Minimum request Left Girder a_{5} or I_{x} (in^{4}) : 6.212 Eff. I_{y} (on^{4}) : 4.896 uency f_{y} (itx) : 5.987	in <i>C_j</i> = 2 uired on the pl Right Girder 7,800 12,294 9.371	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results: It is recomm I _{che} Dynamic Ef	ended that rds (in ⁴) : £ I ₁ (in ⁴) :	Span = Spacing = I _{cheede} of all Joists: 1,634 2,356	40.0 6.0	0 ft 1 ft on center Joist tl edge and Joist Girders be s Ichor Dynamic Natural Freq	Left End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum requ Left Girder Left Girder is or I_n (n^4) : 6,212 : Eff. I_g (n^4) : 4,896	in <i>C_j</i> = 2 wired on the pl Right Girder 7,800 12,294	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef atural Frequen Self-Wei Vibration	ended that $rds(in^4):$ $f_{1}(in^4):$ $cy f_1(Hz):$	Span = Spacing = I _{chareds} of all Joists: 1,634 2,356 6,108 20 er & Joist:	40.0 6.01 Joists a Bay Fr	0 ft 1 ft on center Joist ti odge nd Joist Girders be i Ichan Dynami Natural Free Self- equency f_c: 4.275	Left End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum req Left Girder as or I_x (in^4) : 6.212 Eff. I_a (in^4) : 4.896 uency f_a (in^2) : 5.987 Weight (pl) : 67 Hz	in <i>C_j</i> = 2 uired on the pl Right Girder 7,800 12,294 9.371	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A	:40 :60
Center Joist (j Results: It is recommo I _{clow} Dynamic Ef atural Frequen Self-Wei	ended that $rds(in^4):$ $f_{1}(in^4):$ $cy f_{1}(Hx):$ ight (plf):	Span = Spacing = I _{chareds} of all Joists: 1,634 2,356 6,108 20 er & Joist:	40.0 6.01 Joists a Bay Fr	0 ft 1 ft on center Joist ti dgg nd Joist Girders be s Ichen Dynami Natural Preq Self- equency fn: 4.275 > 0.55%	Left End : 5.00 Right End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum request eff in the Minimum request e	in C _j = 2 wired on the pl Right Girder 7,800 12,294 9.371 135	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef Jatural Frequen Self-Wei Vibration	ended that $rds(in^4):$ $f_{1}(in^4):$ $cy f_{1}(Hx):$ ight (plf):	Span = Spacing = I _{cheerde} of all Joists: 1,634 2,356 6,108 20 rr & Joist:	40.0 6.01 Joists a Bay Fr	0 ft 1 ft on center Joist ti dgg nd Joist Girders be s Ichen Dynami Natural Preq Self- equency fn: 4.275 > 0.55%	Left End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum req Left Girder as or I_x (in^4) : 6.212 Eff. I_a (in^4) : 4.896 uency f_a (in^2) : 5.987 Weight (pl) : 67 Hz	in C _j = 2 wired on the pl Right Girder 7,800 12,294 9.371 135	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef atural Frequen Self-Wei Vibration	ended that $rds (in^4) :$ $ft I_1 (in^4) :$ $cy f_1 (Hz) :$ ght (plf) : Left Girde	$Span = Spacing =$ $I_{cherede} \text{ of all } Joists:$ $1,634$ 2.356 6.108 20 $r \& loist:$ $a_p / g = 0$ $der \& loist:$	40.0 6.0 Joists a Bay Fr 0.538% Bay Fr	0 ft 1 ft on center Joist ti odge nd Joist Girders be s Icher Dynami Natural Freq sequency fa: 4.275 > 0.5% Engineer equency fa: 5.117	Left End : 5.00 Right End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum requests eff I _g (n^4) : 6.212 Eff I _g (n^4) : 4.896 uency f _g (lz) : 5.987 Weight (plf) : 67 Hz (Controls) ing Judgement Required if thi	in C _j = 2 wired on the pl Right Girder 7,800 12,294 9.371 135	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef Jatural Frequen Self-Wei Vibration	ended that $rds (in^4) :$ $ft I_1 (in^4) :$ $cy f_1 (Hz) :$ ght (plf) : Left Girde	$Span = Spacing =$ $I_{cherede} \text{ of all } Joists:$ $1,634$ 2.356 6.108 20 $r \& loist:$ $a_p / g = 0$ $der \& loist:$	40.0 6.0 Joists a Bay Fr 0.538% Bay Fr	0 ft 1 ft on center Joist I codge and Joist Girders be a Icher Dynami Natural Preq Solf sequency fn > 0.55% - 0.55%	Left End : 5.00 Right End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum requests eff I _g (n^4) : 6.212 Eff I _g (n^4) : 4.896 uency f _g (lz) : 5.987 Weight (plf) : 67 Hz (Controls) ing Judgement Required if thi	in C _j = 2 wired on the pl Right Girder 7,800 12,294 9.371 135	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef Jatural Frequen Self-Wei Vibration	ended that $rds (in^4) :$ $ft I_1 (in^4) :$ $cy f_1 (Hz) :$ ght (plf) : Left Girde	$Span = Spacing =$ $I_{chorech} \text{ of all } Joints:$ $1,634$ $2,356$ 6.106 20 tr & Joist: $a_p / g = 0$ lor & Joist:	40.0 6.0 Joists a Bay Fr 0.538% Bay Fr	0 ft 1 ft on center Joist I loist Girders be s Ichen Dynami Natural Preq Solo Solo 4.275 > 0.5% < 0.55% < 0.55% - Engineer equency f_a: 5.117 < 0.5% - OK	Left End \pm 5.00 Right End \pm 5.00 Right End \pm 5.00 his bay parallel to free opening, or exterior \pm No specified as the Minimum request eff Girder a_{t} or I_{π} (in ⁴) \pm 6.212 \pm Eff I_{μ} (on ⁴) \pm 4.896 uency f_{μ} ($H2$) \pm 5.987 Weight (pIf) \pm 67 Hz (Controls) ing Judgement Required if thi Hz	in $C_j = 2$ utired on the pl Right Girder 7,800 12,294 9,371 135 is is Acceptable	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef Jatural Frequen Self-Wei Vibration	ended that $rds (in^4) :$ $ft I_1 (in^4) :$ $cy f_1 (Hz) :$ ght (plf) : Left Girde	$Span = Spacing =$ $I_{chorech} \text{ of all } Joints:$ $1,634$ $2,356$ 6.106 20 tr & Joist: $a_p / g = 0$ lor & Joist:	40.0 6.0 Joists a Bay Fr 0.538% Bay Fr	0 ft 1 ft on center Joist I loist Girders be s Ichen Dynami Natural Preq Solo Solo 4.275 > 0.5% < 0.55% < 0.55% - Engineer equency f_a: 5.117 < 0.5% - OK	Left End : 5.00 Right End : 5.00 Right End : 5.00 his bay parallel to free opening, or exterior : No specified as the Minimum requests eff I _g (n^4) : 6.212 Eff I _g (n^4) : 4.896 uency f _g (lz) : 5.987 Weight (plf) : 67 Hz (Controls) ing Judgement Required if thi	in $C_j = 2$ utired on the pl Right Girder 7,800 12,294 9,371 135 is is Acceptable	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm Icho Dynamic Ef Jatural Frequen Self-Wei Vibration	ended that $rds (in^4) :$ $ft I_1 (in^4) :$ $cy f_1 (Hz) :$ ght (plf) : Left Girde	$Span = Spacing =$ $I_{chorech} \text{ of all } Joints:$ $1,634$ $2,356$ 6.106 20 tr & Joist: $a_p / g = 0$ lor & Joist:	40.0 6.0 Joists a Bay Fr 0.538% Bay Fr	0 ft 1 ft on center Joist I loist Girders be s Ichen Dynami Natural Preq Solo Solo 4.275 > 0.5% < 0.55% < 0.55% - Engineer equency f_a: 5.117 < 0.5% - OK	Left End \pm 5.00 Right End \pm 5.00 Right End \pm 5.00 his bay parallel to free opening, or exterior \pm No specified as the Minimum request eff Girder a_{t} or I_{π} (in ⁴) \pm 6.212 \pm Eff I_{μ} (on ⁴) \pm 4.896 uency f_{μ} ($H2$) \pm 5.987 Weight (pIf) \pm 67 Hz (Controls) ing Judgement Required if thi Hz	in $C_j = 2$ utired on the pl Right Girder 7,800 12,294 9,371 135 is is Acceptable	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	:40 :60
Center Joist (j Results: It is recomm lease Dynamic Ef latural Frequen Self-Wei Yibration	ended that rds (in ⁴) : erf (in ⁴) : ght (pif) : Left Girde Right Gird	$\begin{aligned} &\text{Span} = \\ &\text{Spacing} = \\ &\text{Ichards of all }\\ &\text{Joists:} \\ &1,634 \\ &2,356 \\ &6.106 \\ &20 \\ &\text{or & k Joist:} \\ &a_p/g = \\ &\text{der & k Joist:} \\ &a_p/g = \\ &\text{der & k Joist:} \end{aligned}$	40.0 6.0 Joists a Bay Fr Bay Fr 0.471%	0 ft 1 ft on center Joist I loist Girders be s Ichen Dynami Natural Preq Solo Solo 4.275 > 0.5% < 0.55% < 0.55% - Engineer equency f_a: 5.117 < 0.5% - OK	Left End \pm 5.00 Right End \pm 5.00 Right End \pm 5.00 his bay parallel to free opening, or exterior \pm No specified as the Minimum request eff Girder a_{t} or I_{π} (in ⁴) \pm 6.212 \pm Eff I_{μ} (on ⁴) \pm 4.896 uency f_{μ} ($H2$) \pm 5.987 Weight (pIf) \pm 67 Hz (Controls) ing Judgement Required if thi Hz	in $c_j = 2$ uired on the pl Right Girder 12,294 9,371 135 is is Acceptable to determined	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans.	40 660 mgle
Center Joist (j Results: It is recomm Icise Dynamic Ef latural Frequen Self-Wei Vibration Evaluation:	ended that rds (in ⁴) : rds (in ⁴	Span = Spacing = Ichards of all Joints: 1,634 2,356 6,108 20 or & Joist: $a_p/g = -$ bar & Joist: $a_p/g = -$	40.0 6.0 Joists a Bay Fr 0.538% Bay Fr 0.471%	0 ft 1 ft on center Joist I I dist Girders be i I chorn Dynamin Natural Freq Self- equency fa: 4.275 > 0.5% - Engineer equency fa: 5.117 < 0.5% - OK Floor Bay : Engin	Left End \pm 5.00 Right End \pm 5.00 Right End \pm 5.00 his bay parallel to free opening, or exterior \pm No specified as the Minimum request eff Girder a_{t} or I_{π} (in ⁴) \pm 6.212 \pm Eff I_{μ} (on ⁴) \pm 4.896 uency f_{μ} ($H2$) \pm 5.987 Weight (pIf) \pm 67 Hz (Controls) ing Judgement Required if thi Hz	in $C_j = 2$ uired on the pl Right Girder 7,800 12,294 9,371 135 is is Acceptable to determine D d area to ho would be	Total Load < L/ 2 Live Load < L/ 3 Joist Web Type : A ans. : : : : : : : : : : : : : : : : : : :	40 660 angle

Summary Output:

- 1 page document
- has Inputs & Results
- set-up to go in Engineer's Calculation package
- also part of "Summary & Calc" output



Page 1

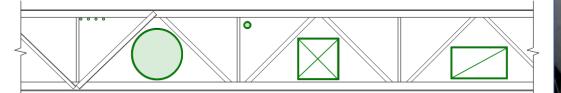
Project: Vibration Analysis - Office Floor Job No. 19-0125 Engineer: JJW Page:					
Vibration Analysis Tool - Walking	25				
References: SJI Technical Digest 5: Vibration of Steel Joist - Concrete Slab Floors 2015 & AISC Steel Design Guide 11: Vibrations of Steel-Framed Structural Systems Dues to Human Activity 2nd Edition 2016	COR	5			
Joists and Girders are both treated as simple span (not continuous) in this tool. Floor Information:	T GROUP	OR			
Bay Info: Line B to C from Line 2 to 9		T GROUP			1
Vibration Occupancy: Office - Electronic	- 3.00 ksi		DR'		Summary & Calc Output:
Total Slab Depth Dead Load = 4.0 psf (including deck) d = 5.00 in Conc. Strength t'_c = 3.00 ksi	:= 145 pcf		GROUP	DR	
Live Load = 8.0 psf Deck Height = 1.50 in Conc. Unit Weight = 145 pcf Collateral Load = 0.0 psf Deck Self-weight = 2.30 psf Canc. Slab Weight = 48.7 psf				GROUP	5 page document
Modal Damping Ratio $\beta = 0.025$ Floor Width = 150.00 ft					1
Constant Force P _e = 65 lb Floor Length = 105.00 ft Girder Information:	effection				has full calculations
eft Girder : 4405N38.4/24K Right Girder : W36X135	libration				
					 set-up to go in
Span = 30.00 ft Span = 30.00 ft oist Girder Deflection Criteria For Girder Tributary Width:					Engineer's Calculation
Total Load < L/ 240 Joist to Left of Left Girder: Span = 40.00 ft Live Load < L/ 360 Joist to Right of Right Girder: Span = 40.00 ft	riteria:	5 Eq. 2.7)			package
	: L/ 240 L/ 360				package
eist Information:	N20 P 41 2000	5 Eq. 2.9)			
enter Joist (joist between girders) 40L/1960/600 Seat Depth Joist Deflection Criteria: Span = 40.00 ft Left End : 5.00 in Total Load < L/ 240		5 Eq. 2.11)			
Spacing = 6.00 ft on center Right End : 5.00 in Live Load < L/ 360					
Joist this bay parallel to free edge, opening, or exterior : No $C_j = 2$ Joist Web Type : Angle					
tesults: It is recommended that the second of all Joists and Joist Girders be specified as the Minimum required on the plans.		G11. Sec. 8.3)			
Joists: Left Girder Right Girder					
I _{chards} (in ⁴): 1,634 I _{chards} or I ₈ (in ⁴): 6,212 7,800 Dynamic Eff. I ₁ (in ⁴): 2,356 Dynamic Eff. I ₈ (in ⁴): 4,896 12,294					
tural Frequency f ₀ (Hz): 6.108 Natural Frequency f ₀ (Hz): 5.987 9.371 Self-Weight (pif): 20 Self-Weight (pif): 67 135					
/ibration Left Girder & Joist: Bay Frequency f.: 4.275 Hz		6 In/sec ²			
valuation: $a_p/g = 0.538\% > 0.5\%$ (Controls) < 0.55% - Engineering Judgement Required if this is Acceptable	Eq. 2.8)	5 Eq. 2.3)			
Right Girder & Joist: Bay Frequency f_{μ} : 5.117 Hz $a_{\mu}/g = 0.471\% < 0.5\% - 0K$	$725\left(\frac{1}{D}\right) \le 0.9$				
			2 0.000		
Floor Bay : Engineering Judgement required to determine if Acceptable		5 Eq. 2.4)	Eq. 3.4)		
alculations based on v1.0, Released 3/2019 Design dated: 5/3/2019	86 in/sec ²			Eq. 3.4)	
e information, calculation and data second or revised it through use of this design tool any present of Stroppen I advantation and you far second on solar or his design tool any professional advantation of the ordinant of the second of the	8 Hz				
mentations, merrarities, and confirms express or register, defined to and inferentian-adolutions of the accessed or ensired Broagh use of the derign trut adolution by the adoluted to accentine mechanisms, the expression processes of an electricity ensure and the processes of a ensired Broagh user of the derign trut adolution by the adolution by the research derign trute adolution of the adolution of the accession of the ensire adding on a derived by the accessed to design to adding of the adolution by the adding of the adolution of the accession of the ensire adding of the adding of	/3/2019		q. 3.6)		
Page 1	5 7 5 6 (K K K K K K K K K K K K K K K K K K	10.0000		ą. 3.6)	
		/3/2019			
]			
			2019		
				2019	
	1.29		2019	2019	
					J

Mechanical, Electrical & Plumbing

Ducts work best when located in middle 2/3 of span.









VULCRAFT/VERCO GROUP

Mechanical, Electrical & Plumbing

ACCESSORIES & DETAILS

- Page 36 of Joist Manual gives Approximate opening sizes
- Ducts with Insulation
 - Compare outside diameter with insulation to table

Joist Depth (in.)	Panel Length (in.)	Round (in.)	Square (in.)	Rectangula (in. x in).
10	19*	5	4	3x6
12	19*	6	5	4x7
14	19*	7	6	5x7
16	19*	8	6	6x7
18	24*	9	7	6x9
20	24*	10	8	7x9
22	24*	10	9	8x9
24	24*	11	9	9x9
18	48	10	8	6x18
20	48	10	8	7x18
22	48	10	9	8x18
24	48	12	10	8x19
26	48	15	12	9x19
28	48	16	13	10x18
30	48	17	14	11x19
32	64	20	16	11x25
34	68	22	18	12x28
36	72	24	18	13x29
38	76	25	20	13x30
40	80	26	22	14x32
42	84	27	22	16x34
44	88	28	23	17x36
46	92	30	24	18x36
48	96	32	26	19x40
50	100	33	27	20x42







Large Openings

- Vierendeel Openings can be done
 - LH, DLH, CJ
- □ Page 37 of Joist Manual
- Locate in mid-third of span
- Possible Cost premium for these
 - If chord angles have to be upsized, there are add'l costs

ACCESSORIES & DETAILS

Vierendeel Openings

Design Considerations:

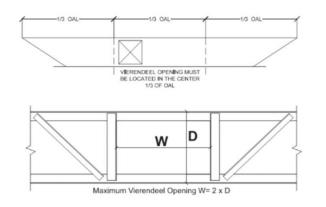
1. As a "general rule of thumb" vierendeel openings can be fabricated with a horizontal width up to 2 times the depth of the steel joist.

2. It is desirable, to locate the vierendeel opening near the mid-span of the steel joist. Doing so reduces the required chord bending moments from transferring the vertical shear forces across the vierendeel opening with no diagonal web members. This decreases the penalty to the top and bottom chord size for the opening.

3. One critical load case is live loading on only half the joist span.

4. It is desirable to avoid multiple vierendeel openings within a joist. Where multiple vierendeel openings are required, the minimum distance between vierendeel openings shall be no less than two times the joist depth.

5. When determining the net available opening dimensions, consideration must be given to fire proofing thicknesses (where it occurs).



Specification

•Call out locations of openings on structural framing plans.

 In addition to width of opening, call out required height of opening so joist chords or joist depth can be adjusted accordingly.

NUCOR

VULCRAFT

WWW.VULCRAFT.COM



V2020J 37





Joists & Decking





Verco Deck: West of Rockies Vulcraft Deck: East of Rockies

VUL

Rebar







Metal Building Systems





Catalogs/Manuals

Catalogs/Manuals can be downloaded

<u>https://vulcraft.com/Literature</u>

□Websites:

- <u>https://vulcraft.com/</u>
- https://vercodeck.com/

Contact Info

Vulcraft or Ecospan engineer contacts:

Darrell Marchell (Northern CA, WA, OR, Western NV): <u>dmarchell@vulcraft-ut.com</u> ; 435-740-0744

John Whiteman (Southern CA, AZ, Southern NV): jwhiteman@vulcraft-ut.com; 714-264-3035

Joe Walton (UT, ID): jwalton@vulcraft-ut.com; 385-272-0744

Scott May: scott@Vulcraft-ut.com; 435-734-4488

SJI Technical Digests

www.SteelJoist.org

- □TD No. 2 Bridging Design
- □TD No. 3 Structural Design of Steel Joist Roofs to Resist Ponding Loads
- □TD No. 5 Vibration of Steel Joist Concrete Slab Floors
- □TD No. 6 Structural Design of Steel Joist Roofs to Resist Uplift Loads
- □TD No. 8 Welding of Open Web Steel Joists
- □TD No. 9 Handling and Erection of Steel Joists and Joist Girders
- □TD No. 10 Design of Fire Resistive Assemblies with Steel Joists
- TD No. 11 Design of Lateral Load Resisting Frames Using Steel Joists & Joist Girders
- □TD No. 12 Evaluation and Modification of Existing Steel Joists and Joist Girders
- □TD No. 13 Design of Composite Steel Joists



VULCRAFT/VERCO GROUP

